

# PXIE MEBT Buncher Cavity

## Pre-Design Review

# Goals

It is an initial phase of the cavity design efforts. The goal is, based on the existing FRS (docbase #1071), to converge of the **technical specifications** for the cavity, define ways how elements of the cavity should be designed, and what fabrication (including brazing and finishing) and acceptance (including low-power intermediate RF measurements) steps are needed for commissioning.

## PXIE docbase #1071

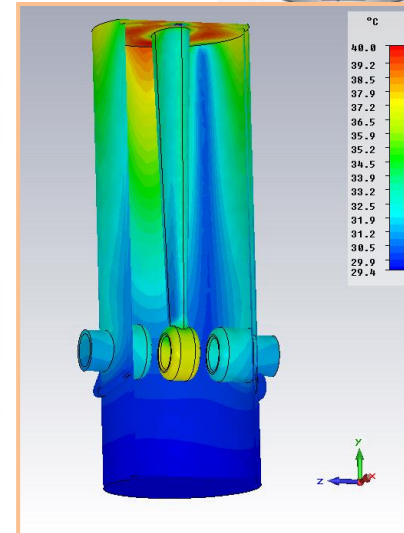
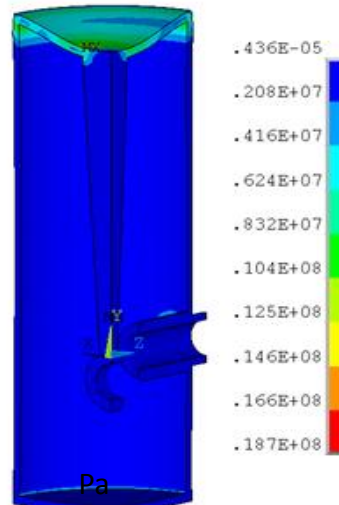
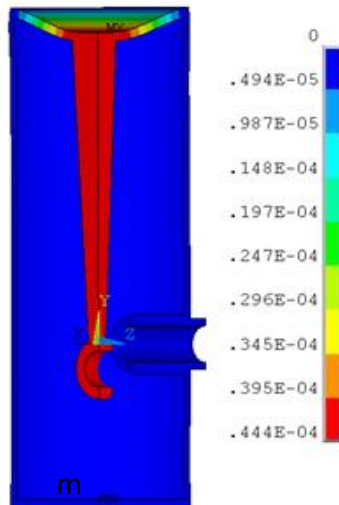
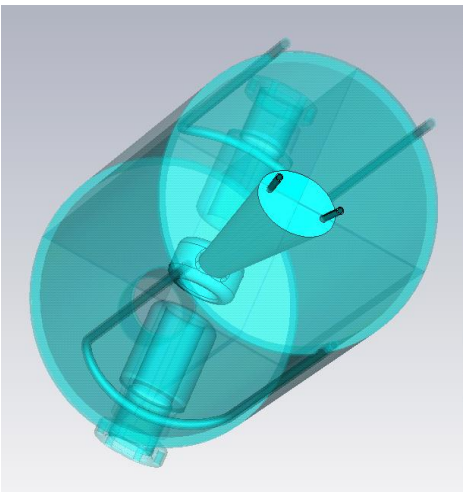
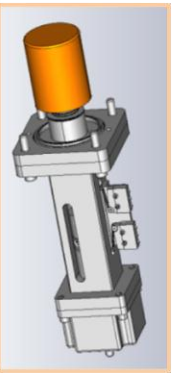
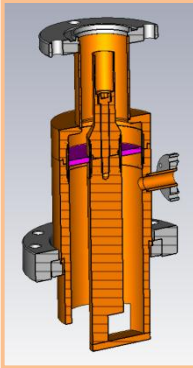
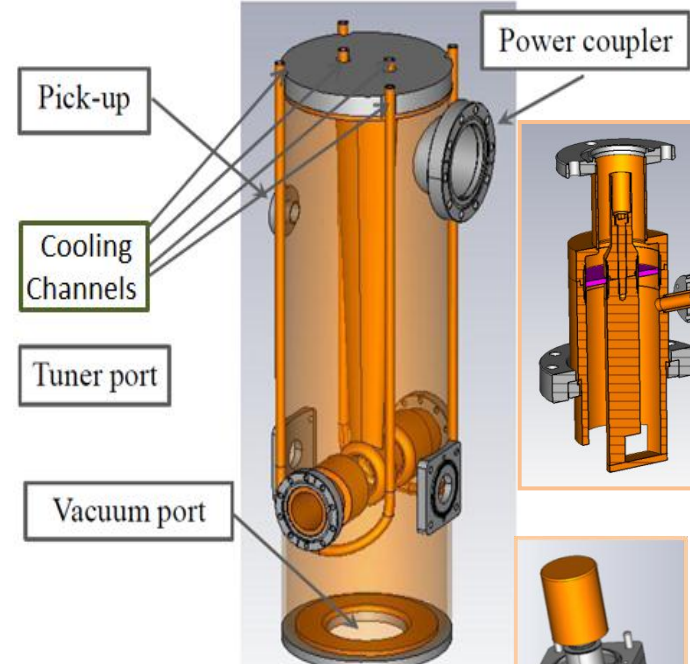
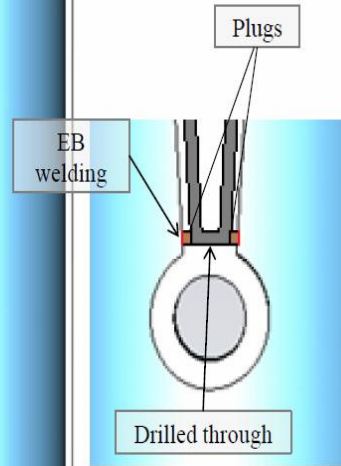
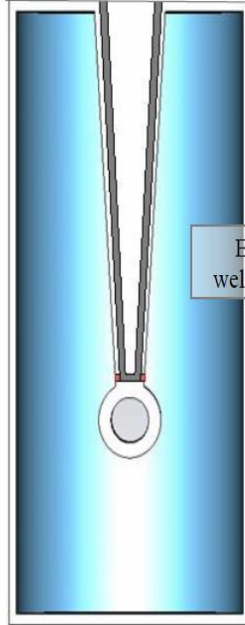
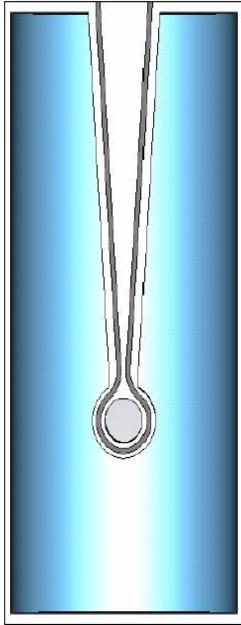
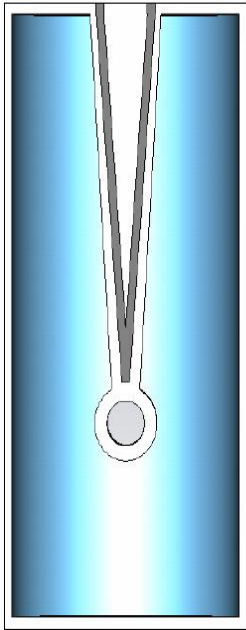
General		
	Minimum beam aperture (ID), mm	30
	Overall module length; flange-to-flange, m	$\leq 0.35$ ← A request to make it smaller
	Positioning accuracy relative to the projected beam trajectory: X, Y, Z, RMS, mm Pitch and Yaw, RMS, mrad	0.5 3
	Cavity vacuum at the operating voltage with no beam, Torr	$\leq 1e-8$ ← Backing, surface finish, pumping speed
Cavity		
	Frequency, MHz	162.5
	Operating mode	CW ←
	Operating temperature, °C	35 ←
	Nominal accelerating voltage at $\beta=0.067$ , MV	0.07
	Maximum accelerating voltage at $\beta=0.067$ , MV	0.10 ← Cooling
	Power loss at maximum voltage, kW	$\leq 3$ ←
	Frequency tuning range, kHz	100
	Maximum water supply pressure, Bar	20 ←

Each cavity must have a provision for use of the next instrumentation:

- Cavity field probe.
- RF coupler e-probe.
- Cavity vacuum monitor

# Status as of June 08, 2012

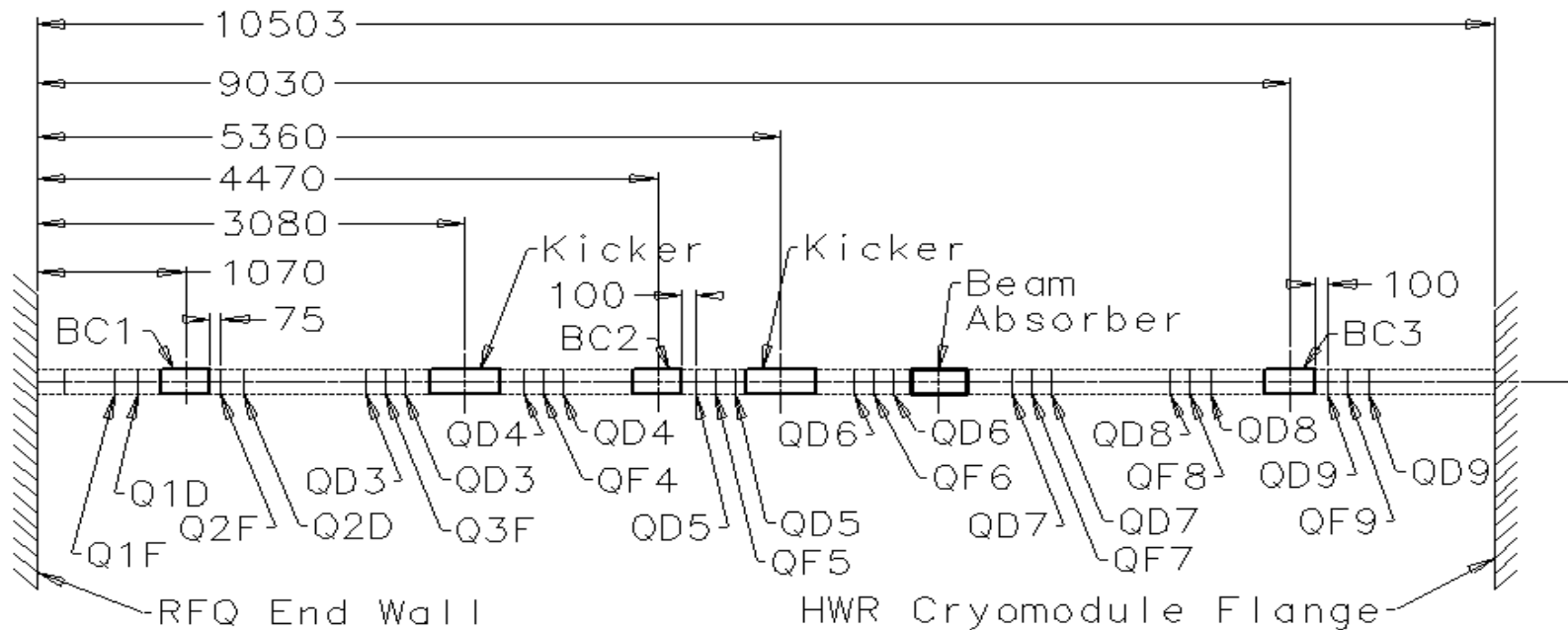
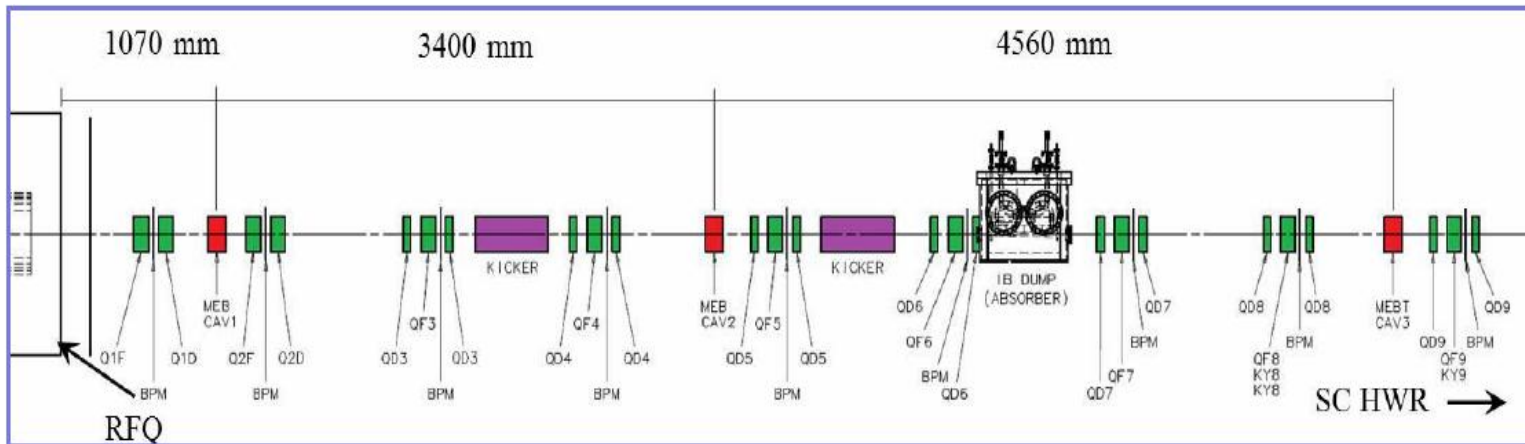
6.9 MPa/ksi



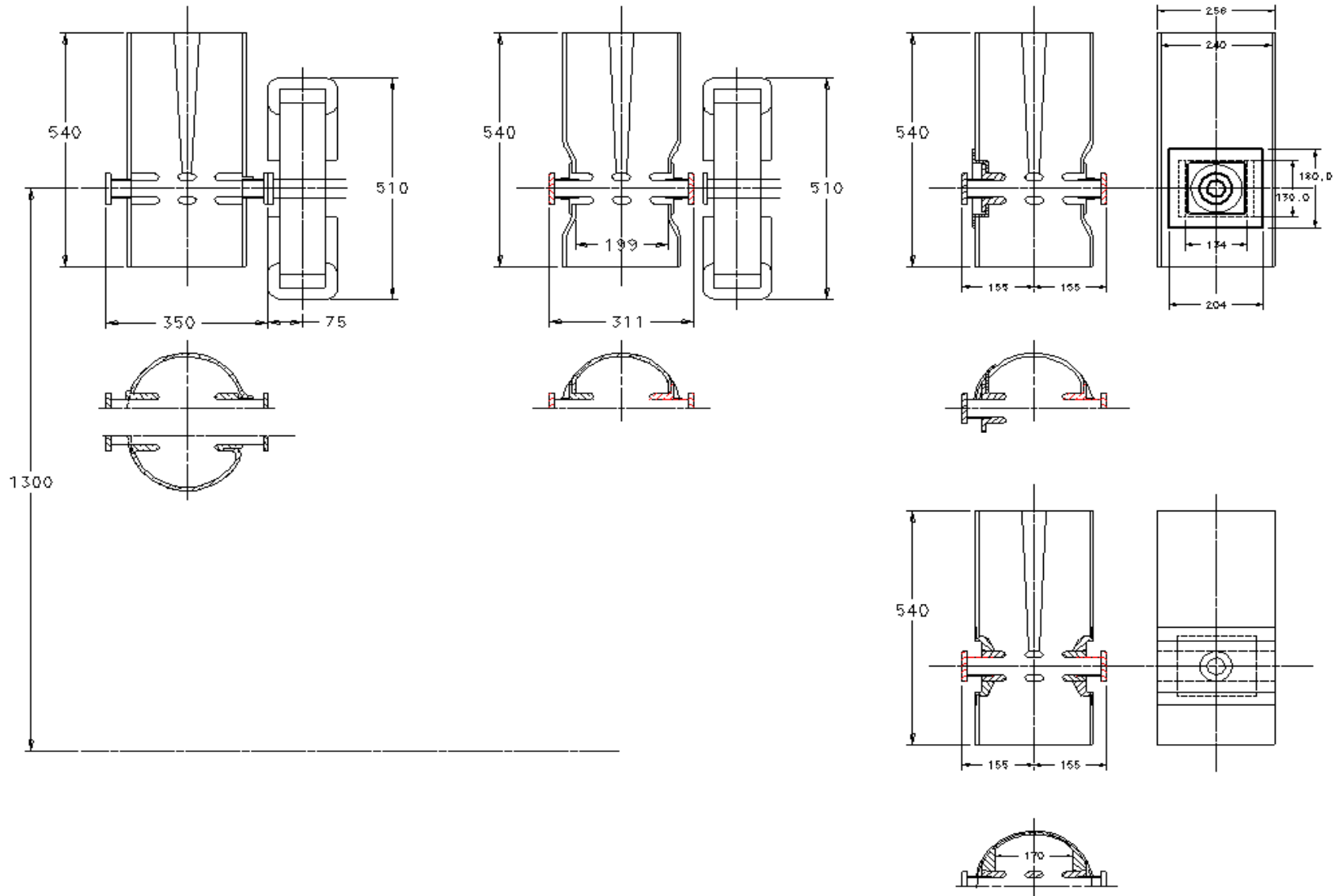
7/10/2012

I. Terechkin

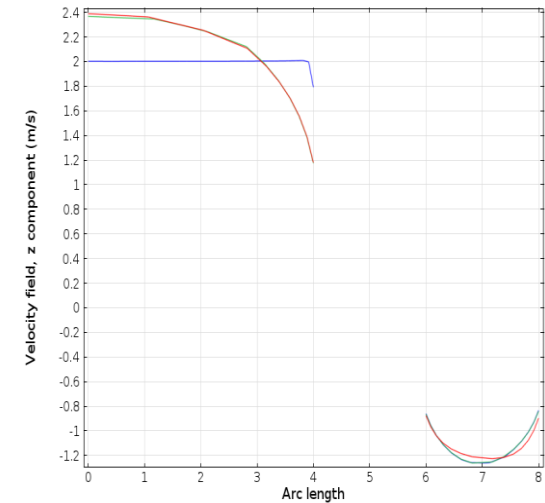
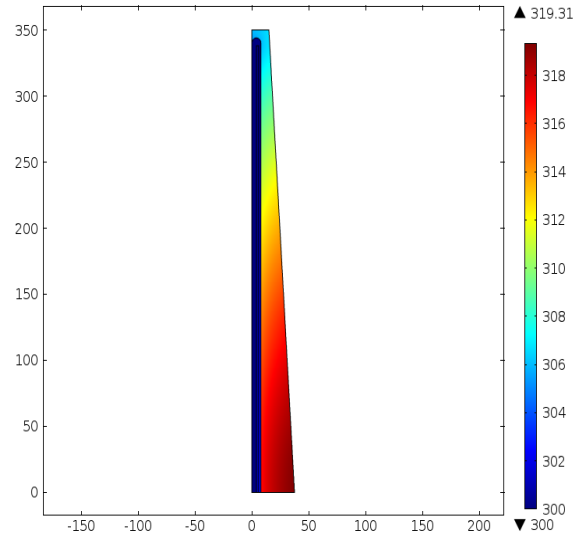
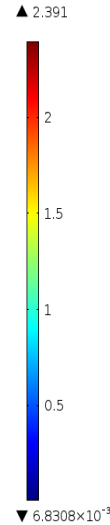
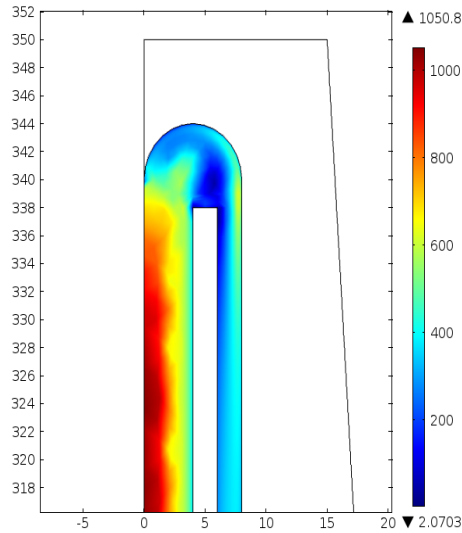
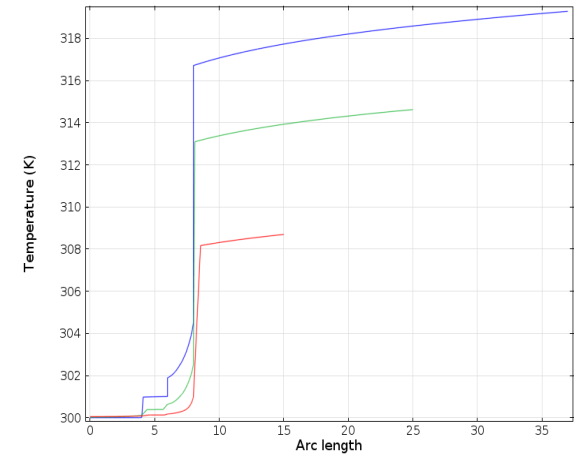
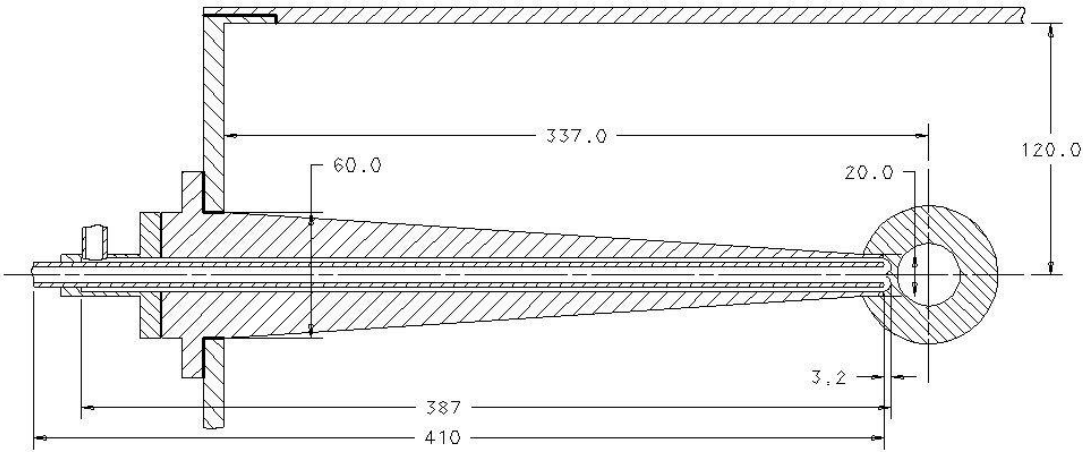
# MEBT Layout



# Integration in the Beam Line



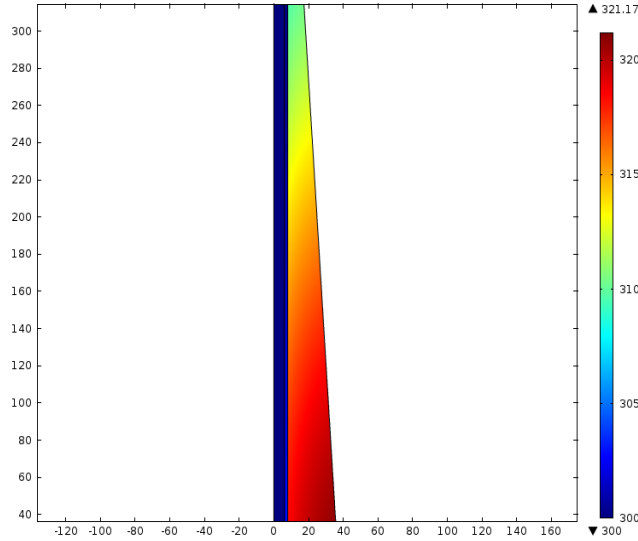
# Central Electrode: Cooling



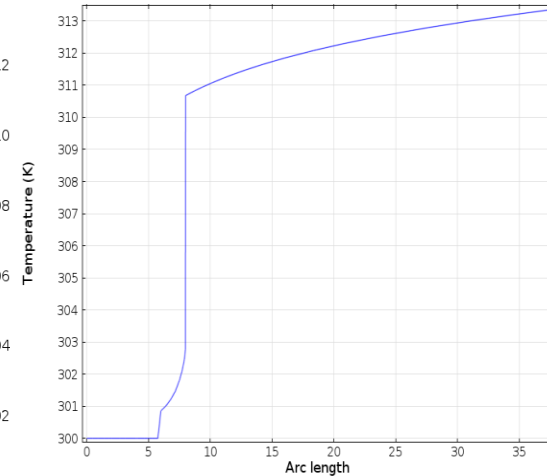
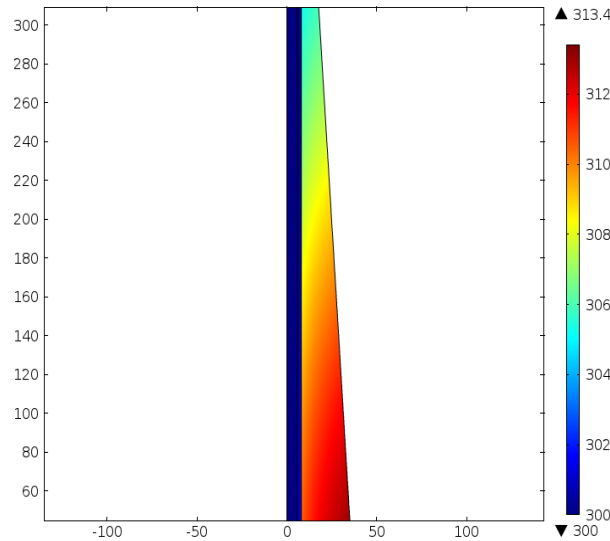
Uniform Heat influx density  $20,000 \text{ W/m}^2$ . Total Heat flux  $\sim 1100 \text{ W}$ .  
Water velocity at the input is  $2 \text{ m/s} \rightarrow 1.6 \text{ GPM}$

# Cooling - Simple

$V = 1 \text{ m/s}$



$V = 2 \text{ m/s}$



$P_{in} = 1206 \text{ W}$

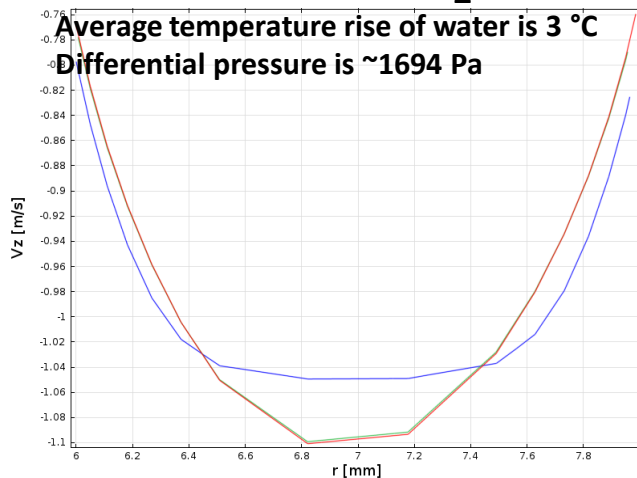
$P_{pipe} = 1095 \text{ W}$

Convective Flux =  $111042 - 110086 = 956 \text{ W}$

Surface area =  $0.0584 \text{ m}^2 \rightarrow P_{in} = 1168 \text{ W}$

Average temperature rise of water is  $3^\circ \text{C}$

Differential pressure is  $\sim 1694 \text{ Pa}$



$P_{in} = 1207 \text{ W}$

$P_{pipe} = 1062 \text{ W}$

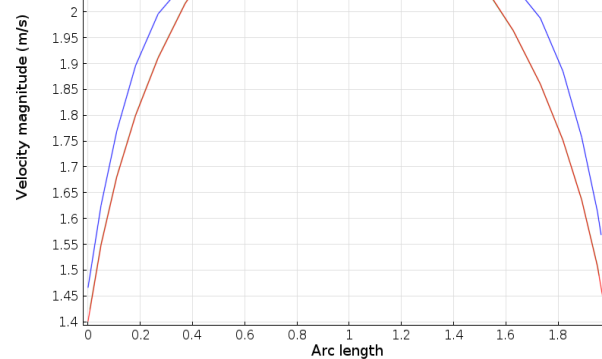
Convective Flux =  $22130 - 220174 = 856 \text{ W}$

Surface area =  $0.0584 \text{ m}^2 \rightarrow P_{in} = 1168 \text{ W}$

Average temperature rise of water is  $1.6^\circ \text{C}$

Differential pressure is  $\sim 5648 \text{ Pa}$

Flow =  $1.75 \times 10^{-4} \text{ m}^3/\text{s} = 0.175 \text{ l/s} \rightarrow 10.5 \text{ l/s} \sim 3 \text{ GPM}$



Adding turbulizators  
reduces the maximum  
temperature by  $\sim 3 \text{ K}$  and  
increases pressure by  
factor of 2



# Simplified Geometry of the Central Electrode

Satisfactory results of the cooling study allow using simplified geometry of the cavity:  
conical stem with round cross-section (Meiyu)

**U = 100 kV**

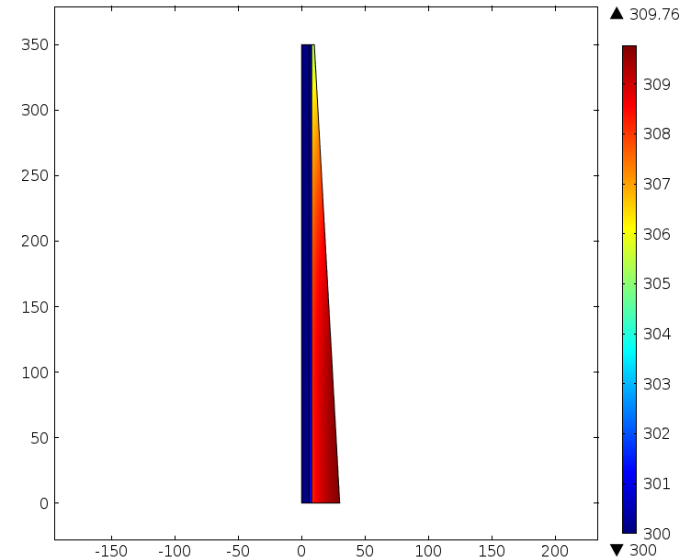
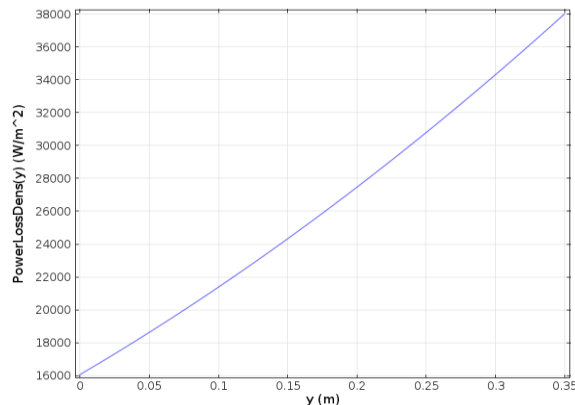
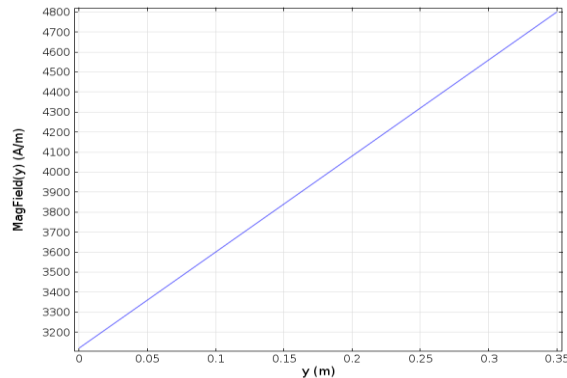
**P = 1100 W on the central electrode**

**v = 2 m/s; Diff pressure in the channel – 5700 Pa**

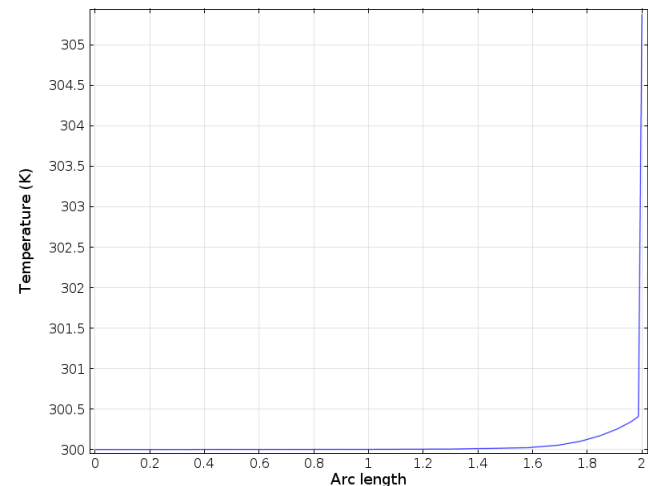
**Water Flux =  $1.76 \cdot 10^{-4} \text{ m}^3/\text{s} = 0.176 \text{ l/s} \rightarrow 2.8 \text{ GPM}$**

**Heat through convection = 860 W**

**Total power loss in the cavity = ~1.5 kW**



Temperature across the channel



# During the Design Stage

1. Get all tuners and power couplers;
2. Decide on a size of all flanges;
3. Decide of the brazing procedure: materials and sequencing;
4. Make a mockup and test water cooling of the central electrode;
5. Define surface finish and fabrication tolerances;
6. Define surface cleaning procedures;
7. Decide on water pressure and flow gauges → buy;
8. Decide on temperature gauges (type and location) → buy;
9. Make a list of potential vendors;
10. Start planning for training and testing;